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Development of high-strength CORC® conductors with record-breaking irreversible axial tensile strain limit exceeding 7 %

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CORC® magnet cables and wires

CORC® wires (2.5 – 4.5 mm diameter)

- Wound from 2 3 mm wide tapes with 25 and 30 μ m substrate
- Typically no more than about 30 tapes
- Flexible with bending down to < 50 mm diameter

CORC® cable (5 – 8 mm diameter)

- Wound from 3 4 mm wide tapes with 30 50 μm substrate
- Typically no more than about 50 tapes
- Flexible with bending down to > 100 mm diameter

CORC®-Cable In Conduit Conductor (CICC)

- Performance as high as 100,000 A (4.2 K, 20 T)
- Combination of multiple CORC® cables or wires
- Bending diameter about 1 meter

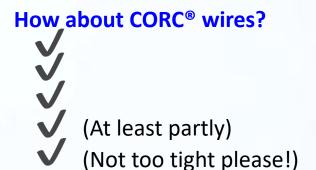




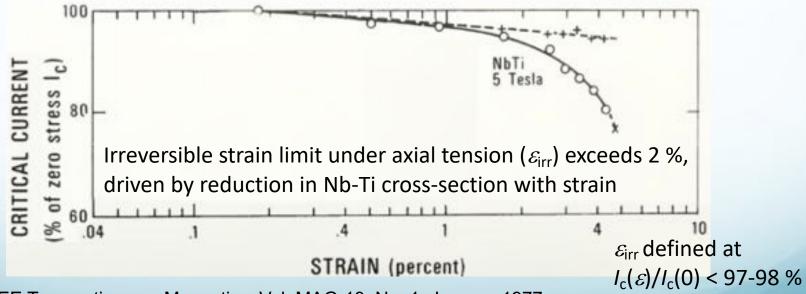
Why is Nb-Ti the workhorse of superconducting magnets?

Nb-Ti is a superconducting magnet workhorse because

- It's a round
- It's fully isotropic (mechanically and electro-magnetically)
- Doesn't require reaction after magnet winding
- It's a transposed, multifilament wire
- It's highly flexible, allowing very tight bends



We know this, so what's new? To find out, let's consider this 44 year old plot:



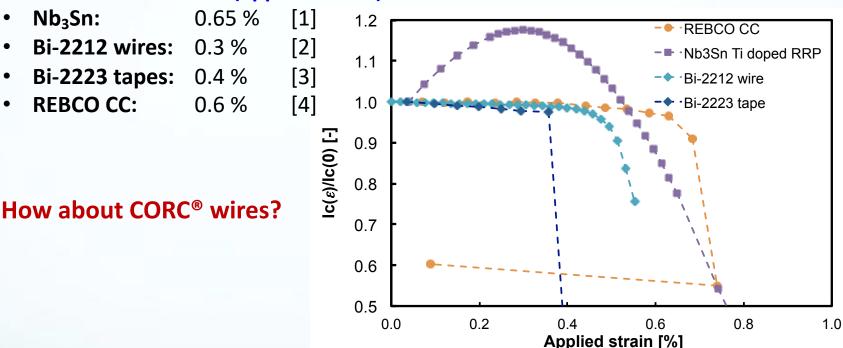
J.W. Ekin, IEEE Transactions on Magnetics, Vol. MAG-13, No. 1, January 1977





Irreversible strain limit of practical superconductors

Irreversible strain limit (applied strain)



- [1] Najib Cheggour, Theodore C. Stauffer, William Starch, Peter J. Lee, Jolene D. Splett, Loren F. Goodrich & Arup K. Ghosh, *Scientific Reports* **8**, 13048 (2018)
- [2] N Cheggour, X F Lu, T G Holesinger, T C Stauffer, J Jiang and L F Goodrich, *Superconduct. Sci. Technol.* **25**, 015001 (2012)
- [3] D.C. van der Laan, J.F. Douglas, C.C. Clickner, T.C. Stauffer, L.F. Goodrich, and H.J.N. van Eck, Supercond. Sci. Technol. **24**, 032001 (2011)
- [4] van der Laan D C and Ekin J W, Appl. Phys. Lett. 90, 052506 (2007)





The effect of axial tensile strain on I_c of CORC[®] wires



Simplified description of CORC® wire structure

- REBCO tapes wound in a helical fashion on solid core
- Tapes behave as springs; extending axially and contracting radially under tensile load
- The core acts a central support, but also confines the radial contraction of the springs

Testing CORC® wires under axial tension

- Test performed in LN₂ at 77 K
- Maximum load of 13 kN applied to terminations
- Sample strain measured with pair of clamp-on extensometers

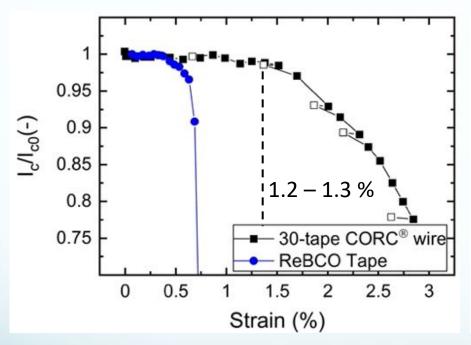


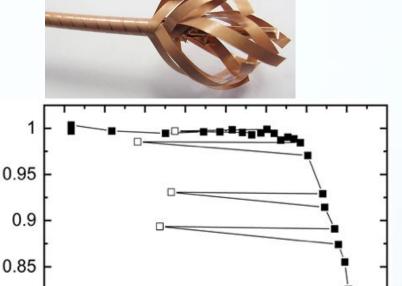


Performance of a standard 30-tape CORC® wire

Standard CORC® wire

- 30 REBCO tapes of 2 mm width
- Annealed copper former (2.55 mm diameter)
- Wire diameter 3.6 mm





Stress (MPa)

- Critical strain is already twice that of a straight REBCO tape
- Critical stress of 150 MPa is competitive with magnet conductors such as Nb₃Sn

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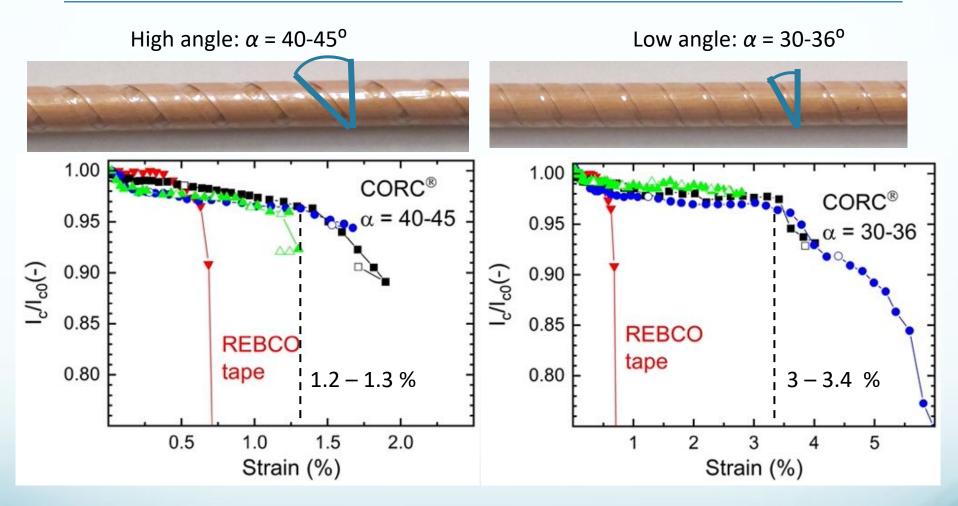
100 125 150 175

0.8

76 K

25

Effect of tape winding angle on ε_{irr}



Tape winding angle drives the irreversible strain limit in CORC® wires

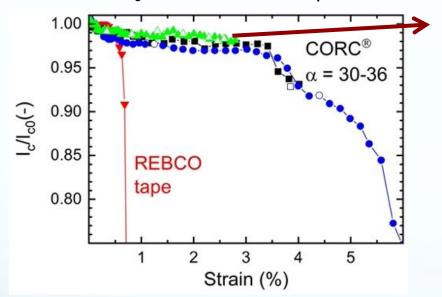




Verification of tape I_c retention after strain

Procedure

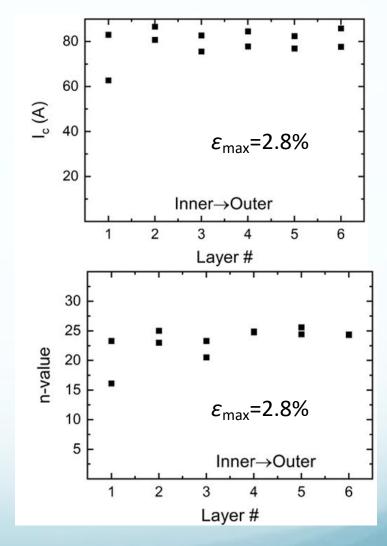
- Strain CORC® wire to 0.85 x ε_{irr}
- Extract tapes from CORC® wire
- Measure I_c from extracted tapes



Results

- CORC® wire retention 98 %
- Extracted tape I_c retention 98 %

High ε_{irr} of 3.3 % is real!



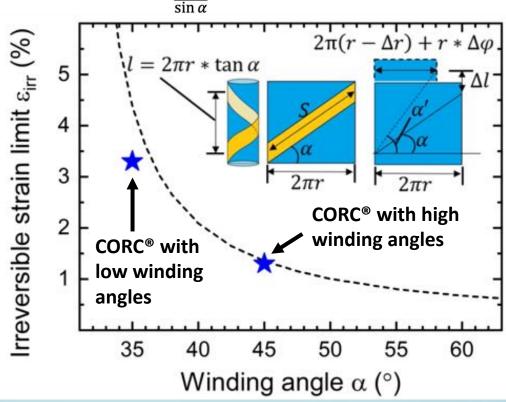


Analytical verification of strain results

Analytical approach

- Calculate the tape axial strain from change in geometry
- Ignore the torsion component

$$\varepsilon_{\text{tape}} = \frac{\Delta S}{S} = \frac{\frac{l + \Delta l}{\sin \alpha'} - \frac{l}{\sin \alpha}}{\frac{l}{\sin \alpha}} \approx \frac{\Delta l}{l} (\sin^2 \alpha - \nu \cos^2 \alpha)$$

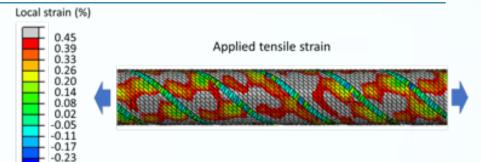


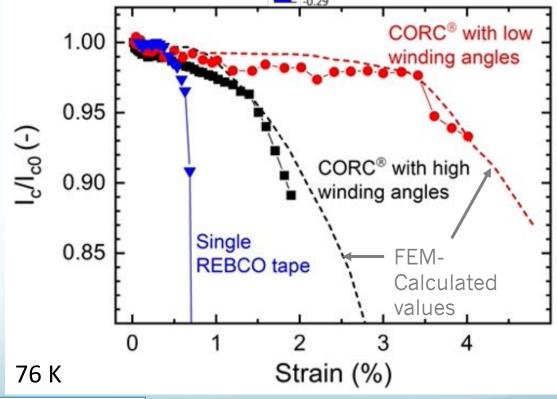


FEM verification of results

FEM approach

- Calculate REBCO value exceeding $\varepsilon_{
 m irr}$
- Assumes I_c correlates to remaining superconducting volume





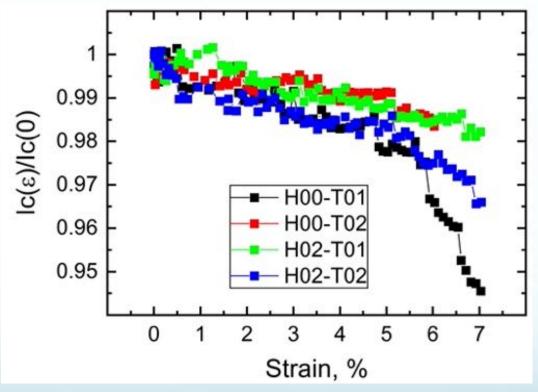




Extending ε_{irr} of high tape count CORC® wires

Optimized 28-tape CORC® wire layout

- 28 tapes of 2 mm width (30 μm substrate)
- 14 layers wound on 2.55 mm copper former
- tape winding angle 25 35°, depending on layer



Optimized 28-tape CORC® wire : $\varepsilon_{irr} = 6 - 7 \%!!$

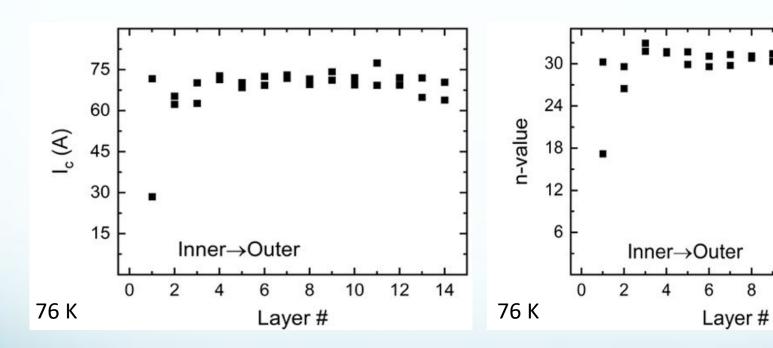




Verification of tape I_c retention after high strain

Optimized 28-tape CORC® wire

- CORC® wire I_c retention 98 % at 7 % strain
- Extracted tape I_c retention 99 %
- Only tapes in the inner layer are damaged



Irreversible strain limit in CORC® wires can be increased significantly by minimizing the tape winding angle



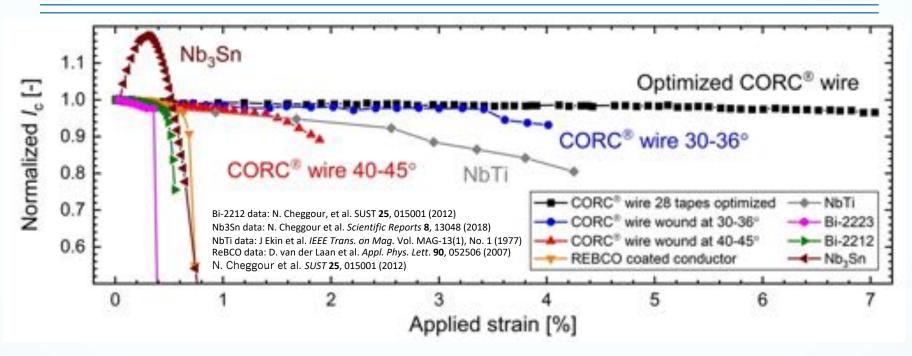


10

12

14

Axial strain practical superconductors Master Plot



CORC® wires can now be engineered to have ε_{irr} :

- twice as high as Nb-Ti
- 10 times as high as REBCO coated conductors
- 20 times as high as Nb₃Sn, Bi-2212 and Bi-2223

Accepted for publication: van der Laan *et al.* "High -temperature superconducting CORC® wires with record-breaking axial tensile strain tolerance present a breakthrough for high-field magnets" DOI https://doi.org/10.1088/1361-6668/ac1aae

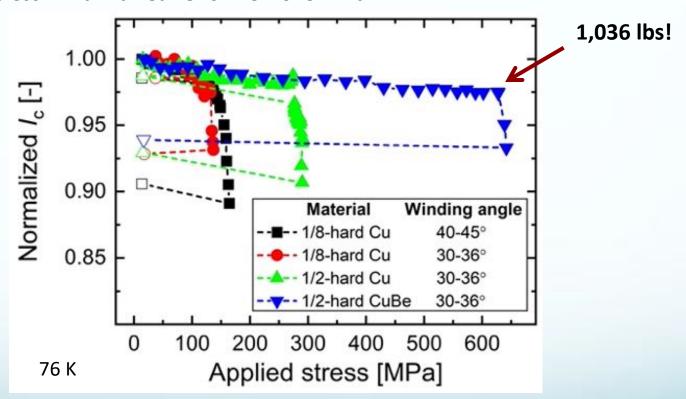




CORC® wires with improved mechanical tensile strength

Critical stress limit under tension (12-tape CORC® wire)

- Critical stress limit with soft annealed copper former: 134 MPa
- Critical stress limit with half hard copper former: 280 MPa
- Critical stress limit with CuBe former: 613 MPa



Irreversible tensile stress limit of CORC® wires can be engineered to exceed 600 MPa at 77 K





Summary

The helical winding of REBCO tapes is CORC® wires allows

- To mechanically decouple the ceramic REBCO film from the CORC® wires
- Reduce the strain transfer from the CORC® wire to the REBCO film
- Allow the irreversible strain limit under axial tension in CORC® wires to far exceed that of the REBCO tape
- This allows extremely high irreversible strain limits in CORC® wires of 7 %

Optimized CORC® wires have an irreversible strain limit under tension

- More than 10x that of REBCO tapes
- More than 20x that of other HTS and Nb₃Sn
- Double that of NbTi

Mechanically decoupling of the REBCO layer allows

- The CORC® wire strength under axial tension to be determined almost entirely on that of the former
- CORC® wires with very high critical stress exceeding 600 MPa at 77 K have been demonstrated



